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ADJUSTING DEVICE

Description

Field of the invention

5 The invention relates to an adjusting device for adjusting a camshaft relative to
10 a camshaft gear wheel driven by a crankshaft, wherein parts provided for the
adjustment procedure are arranged on the camshaft gear wheel and on the
camshaft, according to the preamble of Claim 1.

15 Among other things, stepper motors, which enable self-locking and an exact,
but merely discrete, i.e., non-continuous, adjustment, can be used as adjusting
devices. Furthermore, for achieving self-locking and a high gear reduction, a
worm gear pair can be used. However, for a relatively large amount of friction,
worm gear pairs exhibit low efficiency and require materials that are resistant
to wear and heat.

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DE 195 08 328 A1 presents a self-locking adjusting device for rotating two
bracing parts relative to each other. One of the two bracing parts comprises
internal gearing, into which locking bars or teeth can be inserted in a straight-
line radial direction. The teeth are guided in chambers between webs of the
25 other bracing part, such that the radially inwards and outwards movement is
precisely enabled. The teeth are supported inwards on a control surface, which
is formed as an outer surface of an egg-shaped control element. When the
control element rotates, the teeth are thus periodically pushed outwards in the
radial direction, wherein a few of the teeth engage in the teeth gaps. The outer

end sections of the teeth and the recesses or teeth gaps of the internal gearing taper outwards, so that the teeth transfer torque between the webs of the second bracing part and the internal gearing of the first bracing part for eccentric insertion into a recess.

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However, a disadvantage in this adjusting device is first that only partial self-locking is achieved. When torque acts upon the bracing part with internal gearing, only the one or two teeth, which are pressed against the eccentric region of the control element by the teeth of the internal gearing, contribute to the self-locking effect, depending on the engagement situation of the teeth. The opposing teeth likewise contribute minimally to the self-locking, like those teeth, which are in the radially outer position, i.e., positive-fit in the recess, and those teeth, which are in the radially inner position, i.e., not engaged in the teeth gaps of the internal gearing. However, the possibly only one tooth, which is to contribute to the self-locking effect, can transfer a force not directed towards the rotational axis from the internal gearing to the control element between the point of application of the internal gearing at its outer contact surface and its inner contact surface contacting the control element, which thus leads to transmission of torque. In this way, especially for the use of only a few teeth, no positive-fit connection between the internal gearing and the webs and thus, at least for an unfavorable engagement situation of the teeth, also no complete self-locking can be achieved.

Furthermore, a play-free configuration of such an adjusting device is problematic. The teeth that can move linearly in the radial direction slide with their side surfaces on the side surfaces of the webs of the second bracing part. However, a play-free arrangement of the teeth between the webs is practically impossi-

ble; for achieving a low-friction guidance of the teeth between the webs, a certain overdimension is necessary. Finally, due to the manufacturing-specific tolerances, play between the control surface and the tooth remains even in the positive-fit engagement of a tooth in its radially outer position in a recess of the internal gearing.

Camshaft adjusters are used especially for engine speed-dependent and load-dependent adaptation of the valve opening and closing times for an internal-combustion engine in order to improve the filling. The camshaft is driven by the crankshaft, e.g., by means of toothed belts, a roller chain, or spur pinions, on a camshaft gear wheel, to which the camshaft is connected. The camshaft adjustment is realized by rotating the camshaft relative to the camshaft gear wheel, wherein the transfer of torque must also be guaranteed during the adjustment. Therefore, adjusting devices with high, continuous adjustment accuracy and reliable self-locking are required in all situations. For this purpose, in conventional camshaft adjusting devices, a control piston adjusts against a spring force in a flanged shaft connected to the camshaft through, e.g., a hydraulic drive, wherein the flanged shafts are connected to the camshaft gear wheel and, if necessary a positioning piston, by means of oblique gearing. However, such a configuration is complicated, expensive, and subject to maintenance. Furthermore, complicated feed lines from a central hydraulic pump are required in the vehicle.

The invention is based on the objective of providing an adjusting device, which ensures self-locking and at least essentially play-free, continuous adjustment of two parts for simple and smooth-running operability. Advantageously, a high gear reduction should be achievable.

This objective is met by the features of Claim 1. The subordinate claims describe preferred improvements.

- 5 According to the invention, the teeth thus execute rotational movements during the adjusting movement. These movements of the teeth in general can be superimposed movements of a linear movement directed outwardly and inwardly in the radial direction and a rotational movement of the teeth about a rotational axis parallel to the rotational axis of the parts. In an especially
10 preferred way, the teeth each run on a circular arc path from their inner contact with the drive element to the outer contact with the internal gearing and back on another circular arc path.

- The rotational movements of the teeth according to the invention permits a
15 good adaptation of the shape of the teeth and webs, as well as the internal gearing, to the course of movement, which enables a self-locking engagement of a part of the teeth. In this way, in particular, a more favorable transfer angle between the moving tooth and the internal gearing is achieved, in which the force transfer from the moving tooth to the internal gearing is realized with a
20 small radial part, so that a higher efficiency can be achieved. Furthermore, in particular a defined contact of a tooth to the two adjacent webs is enabled, which leads to a reduction of the play.

- Advantageously, in this way, in the outermost radial position of a tooth, there is
25 no contact with the internal gearing in order to guarantee a defined contact with the adjacent webs also in the position. The coupling of the teeth to the internal

gearing is thus realized at the preferably oblique tooth faces, wherein at least one tooth contacts a front or back tooth face in the rotational direction.

An eccentric is preferably provided as a drive element for adjusting the teeth.

5 For this purpose, an eccentrically mounted circular disk is mounted directly on the input shaft. The teeth contact the outer surface of this circular disk with their inner contact surfaces. However, advantageously as an extension, an eccentric ring is provided between the eccentric disk and the inner contact surfaces of the teeth. Here, the eccentric ring essentially executes a wobble
10 movement without rotation, so that a drive of the teeth is enabled without a frictional connection of their inner contact surfaces to the eccentric ring. The teeth merely roll with slight roller friction on the eccentric ring, so that a higher efficiency is achieved.

15 To achieve a defined contact of the teeth to the drive element, these are advantageously biased in the radial direction. This can be realized in one method through biasing towards the rotational axis, which, e.g., is exerted by a biased elastic O-ring, e.g., a rubber ring. Here, the O-ring can surround axial projections or regions of the teeth, wherein it can also be set, e.g., through
20 recesses of the teeth. Furthermore, biasing can be realized outwardly. This biasing can be realized, e.g., through a biased spring element, which sits on the shaft and presses the eccentric disk in a direction radially outwardly. Here, the spring element can be deformed purely elastically or mounted in the adjusting device under partial plastic deformation. Furthermore, radial biasing outwards
25 is also possible, e.g., through an overdimension. However, in principle biasing is not required.

The rotational movement of the teeth can be initiated advantageously by a control surface at their radially inner reverse point acting as the bottom dead center. The control surface comes into contact with the inner contact surfaces of the teeth, when these are in their radially inner positions. In this way, in particular, a jamming effect of the teeth in the bottom dead center of their movement can be avoided. The control surface can be especially a control gearing region of a control gear wheel rotationally fixed to the second part or embodied integrally with this part. In particular, external gearing can be used as the control gearing. Here, the inner contact surface of a tooth comes into engagement with tooth gaps or recesses of the external gearing of the second part. Instead of external gearing, internal gearing can also be provided accordingly.

The tooth can, according to one embodiment, be turned about a rotational point defined on the first part, in that a tab of the tooth engages in a corresponding guide in the chamber between the webs of the other part. The guide tapers inwards in the radial direction in order to guarantee the defined rotational point at the radially inner position of the tooth and to enable both the inwardly directed, and also the outwardly directed circular arc path at the radially outer positions, in which the side surfaces of the teeth slide in a defined way on the side surfaces of the webs.

Alternatively, the teeth and webs can also have shoulder regions, which ensure the defined rotational movement for the sliding movement of the teeth on the webs.

Furthermore, here a control disk with a control surface creating a frictional connection with the inner contact surfaces of the teeth can also be provided, which is fixed, e.g., rotationally, to the input shaft or to the drive element.

- 5 The adjusting device according to the invention is robust and can transfer high torque forces with reliable self-locking and can guarantee precise position adjustment. Through the favorable transfer angle between the moved tooth and the internal gearing, a high efficiency can be achieved. Advantageously, a high gear reduction is achieved, so that the use of fast-running, small-sized, and
10 cost-effective motors with small output torque is possible.

The adjusting device according to the invention is formed as a camshaft adjusting device, which adjusts the camshaft relative to a camshaft gear wheel driven by the crankshaft. Here, an activation of the input shaft is required only
15 for the adjustment process; no activation or power is required in the corresponding positions due to the self-locking.

The invention is explained in more detail in the following with reference to the attached drawings using a few exemplary embodiments. Shown are:

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Figure 1 an exploded view of an adjusting device according to an embodiment of the invention;

Figure 2 a cross section of the adjusting device according to Figure 1;

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Figure 3 a longitudinal section of the adjusting device according to Figure 1;

Figure 4 a perspective view of the assembled adjusting device;

5 Figures 5a, b a front view and side view of a tooth according to the invention used in the adjusting device;

Figure 6 a cross section with illustration especially of the teeth engaging in the internal gearing;

10 Figure 7 a cross section or superimposed view, especially of the teeth engaging in the external gearing;

Figures 8a-d the representation of the movement of a tooth between adjacent webs;

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Figures 9a-d the representation of the movement of a tooth between the internal and external gearing;

Figures 10a-c front, side, and rear views of the second part;

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Figures 11a-c front, side, and rear views of the first part;

Figure 12 disassembled representation of the device for adjusting a cam-shaft;

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Figure 13 a cross section of an adjusting device according to another embodiment of the invention.

According to Figure 1, as a first part an adjusting device 1 has a first flange part 2, which can be connected to a camshaft via attachment holes 2.1. The first flange part 2 has a center hole 2.2 and webs 2.3, which are spaced apart from each other in the peripheral direction, which project in the axial direction, and between which chambers 2.4 are defined. A second flange part 3 acting as a second part has attachment holes 3.1 for mounting on a camshaft wheel and internal gearing 3.2 with teeth 3.3 and recesses 3.4 formed between the teeth 3.3. An input shaft 4 has a square region 4.1, in which, on two opposing sides, spacing holders 4.4 are set and on another side an elastic (possibly also with additional plastic biasing), tensioned biasing spring element 4.3 is set. A circular disk 4.2 with square center hole 4.5 is set on the spacing holders 4.4 and the biasing spring element 4.3. The disk 4.2 is pressed radially outwards by the biasing spring element 4.3 and is used in its eccentric position as an eccentric disk 4.2. The spacing holders 4.4 glide on the square region 4.1 and/or on the eccentric disk 4.2.

An eccentric ring 6 is set around the eccentric disk 4.2 and executes a wobble movement when the input shaft 4 rotates. Teeth 7 are distributed in the peripheral direction such that with their inner contact surfaces 7.4 they contact the eccentric ring 6 and extend away from the rotational axis A. Outer contact surfaces 7.5 of the teeth 7 engage in the internal gearing 3.2 of the second part 3 when the input shaft 4 rotates. Through the biasing of the biasing spring element 4.3, the teeth 7 are pressed into the internal gearing 3.2. An O-ring 8 is set with biasing around axially extending projections 7.1 of the teeth 7 and creates a contact between each tooth 7 with its inner contact surface 7.4 and the outer side of the eccentric ring 6. In principle, the biasing by the O-ring 8 or by

the biasing spring element 4.3 (and the projections 7.1) can be eliminated, because one of the two biasing means is sufficient. A biasing ring 10 is used for pressing the parts in the axial direction.

5 The guidance of the teeth 7 in the chambers 2.4 between the webs 2.3 can be seen especially in Figure 2 and Figures 8 and 9, because the teeth 7 are in various successive engagement positions for the rotating eccentric disk 4.2. The lowermost tooth 7 in Figure 2 is in the innermost position in the radial direction, at which it contacts the apex point of a tooth 3.3 of the internal
10 gearing 3.2 with its outer contact surface 7.5. Here, the tooth 7 extends precisely in the radial direction. The uppermost tooth 7 in Figure 2 is in its outermost position in the radial direction, at which it is in engagement with a recess 3.4 (tooth gap) of the internal gearing 3.2. Torque is applied to this tooth 7, as well as the other teeth approximately in the bottom half shown in Figure
15 7, through the external gearing 5.2, which creates a defined tipping of the tooth in the innermost position acting as the bottom dead center of the inwards and outwards movement of the teeth. Between the innermost and outermost positions, the teeth 7 move on circular arc paths. The teeth 7 taper according to Figure 5 from the inner contact surface 7.4 to the outer contact surface 7.5,
20 which can be embodied flat or also curved as shown. Side surfaces 7.6 of the teeth advantageously have concave side surface regions 7.7. The teeth 7 glide according to Figure 8 with their side surfaces 7.6 essentially with the concave side surface region 7.7 on the webs 2.3. The webs 2.3 taper towards the rotational axis A, are formed essentially with a triangular or wedge shape, and
25 likewise advantageously have concave side surface regions 2.6.

In the chambers 2.4, additional guides 2.7 are formed as recesses, in which axially projecting tabs 7.9 of the teeth 17 engage. The tabs 7.9 are arranged approximately in the center of the teeth 7 and extend in the axial direction opposite to the projections 7.1 arranged at the bottom end of the teeth 7. The guides 2.7 taper towards the rotational axis A, so that the tabs 7.9 are held in the innermost position of the teeth 7 essentially play-free and form a defined rotational point for the teeth 7. The circular arc-shaped outwards and inwards movements of the teeth 7 are enabled by the expansion of the guides 7.7 outwards.

The external gear wheel 5 is embodied rotationally fixed or integrally with the second flange part 3. In the representations of Figures 2 and 7, the external gear wheel 5 and the eccentric ring 6 are drawn overlapping. The external gearing region 5.2 of the external gear wheel 5 with teeth 5.3 and recesses 5.4 (tooth gaps) formed in-between is used as a control surface. The number of tooth gaps 5.4 of the external gearing 5 can be, e.g., higher by one than the number of teeth 7 and the number of teeth 7 in turn can be equal to the number of webs 12.3 and less by one than the number of teeth 3.3 of the internal gearing 3.2 of the second flange part 3. The inner contact surfaces 7.4 of the teeth 7 come in contact with side faces of the teeth 5.3 of the external gear wheel 5 near their radially inner position, i.e., at the bottom teeth of Figure 2 or the teeth 7 shown in Figure 7.

Through the positive-fit holding of the inner contact surfaces 7.4 of the teeth 7 on the external gear wheel 5, a defined rotation of the teeth 7 at its innermost position corresponding to a bottom dead center is achieved; alternatively, a frictional-connection contact of the teeth 7 on a control disk fixed rotationally,

e.g., to the input shaft 4, is also possible. This results in a continuous support of the teeth 7 on the eccentric ring 6, which acts as a drive element and through which a functional separation of the driving effect and the control surface creating the rotation or tipping of the teeth is achieved.

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According to the embodiment of Figure 12, the second part 20 is formed integrally with the camshaft and the first part 30 is formed integrally with the camshaft wheel 30.

10 For the embodiment shown in Figure 18 [sic: 13], essential parts correspond to those of the first embodiment and therefore are not described in more detail. The adjusting device has teeth 27 with lateral shoulder regions 27.1 and webs 22.3 with lateral shoulder regions 22.4, which come into contact with each other in the gliding movement of the teeth 27. Through the shaping with the
15 shoulder regions, the movement of the teeth can be defined sufficiently, so that in contrast with the embodiment of Figures 1 to 11, the slot-peg guide can be eliminated. Thus, the entire guide and force transfer occurs in a plane, e.g., tipping moments acting on the teeth out of the plane can be prevented. Also for this embodiment, an external gear wheel 15 is provided as a control gear
20 wheel. This external gear wheel engages the bottom regions of the teeth 27 with its external gearing 15.2.

According to the invention, the external gear wheel 5 or 15 can also be decoupled from the driven shaft and supported, e.g., so that it rotates freely.

25 For such an arrangement, the teeth 7 or 27 drive the freely rotating external gear wheel 5 for its inwards movement and are turned by the external gear wheel.

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